

# (In)efficacy of Architected Auxetic Materials for Impact Mitigation: Investigations of Energy Absorption and Force Distribution

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$E_y = 2.49 \text{ GPa}$ ,  $m = 5.5 \text{ g}$



$E_y = 2.49 \text{ GPa}$ ,  $m = 5.98 \text{ g}$



$E_y = 2.48 \text{ GPa}$ ,  $m = 3.99 \text{ g}$



$E_y = 2.49 \text{ GPa}$ ,  $m = 4.12 \text{ g}$

## Background

Auxetic materials are claimed to offer beneficial capabilities for impact mitigation, such as higher indentation resistance and energy absorption. To further investigate the load-transmission characteristics four architectures are compared:

- auxetic re-entrant honeycomb
- rotated auxetic re-entrant honeycomb
- conventional honeycomb (W)
- conventional honeycomb (L)

(see Fig. 1 for unit cells)

## Physical Modeling

- patches of approx.  $130 \text{ mm} \times 65 \text{ mm}$  manufactured and impacted by  $1.2 \text{ kg}$  plungers at  $70 \text{ m s}^{-1}$  (see Fig. 2)
- the auxetic and rotated auxetic structures show high peak loads (see Fig. 3)
- both conventional honeycombs (W and L) show more spread out loading (see Fig. 3)

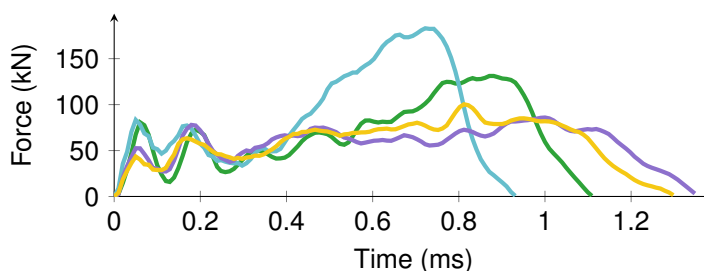


Figure 3: Force on the back-face over time from experiments

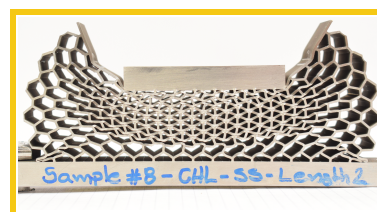
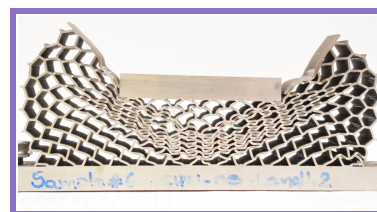
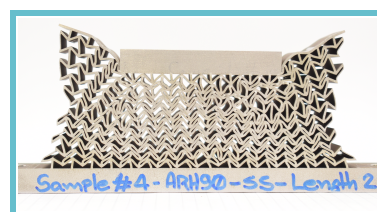
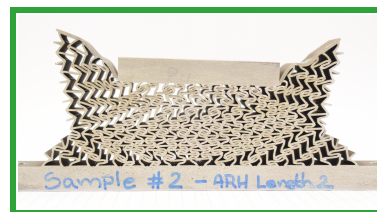


Figure 2: Test samples after the experiments

Figure 1: Investigated unit cells

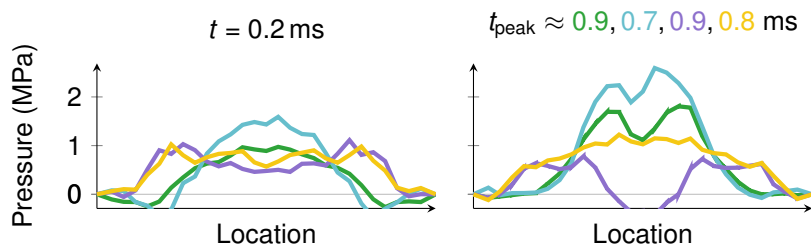


Figure 4: Pressure over the back-face from simulations

## Numerical Modeling

- numerical experiments using ABAQUS to extract forces at arbitrary locations
- material densification in auxetics leads to force densification (see Fig. 4)
- material spread leads to load spread in conventional honeycombs
- effect observable throughout the loading

## Further Investigations

- Design studies using fast, beam-based FEA are being conducted
- Initial results showcasing elastic effects available



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