

# Architectural Choices for Auxetic Metamaterials and their Effects on Impact Mitigation

27<sup>th</sup> Engineering Mechanics Symposium – Hotel Papendal, Arnhem

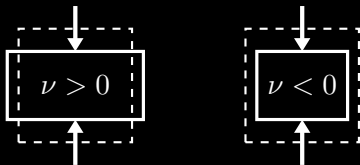
Til Gärtner<sup>ab</sup>   S.J. van den Boom<sup>b</sup>   J. Weerheijm<sup>a</sup>   L.J. Sluys<sup>a</sup>

a. Delft University of Technology

b. Netherlands Institute for Applied Scientific Research (TNO)

# Auxetic materials appear promising for impact mitigation

- auxetic materials are materials with a negative Poisson's ratio
  - materials that contract laterally when compressed

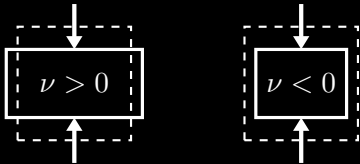


non-auxetic and auxetic materials  
(Lim 2015)

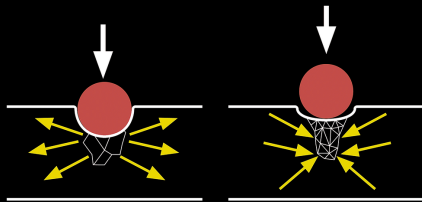


# Auxetic materials appear promising for impact mitigation

- auxetic materials are materials with a negative Poisson's ratio
  - materials that contract laterally when compressed
- promising capabilities for impact mitigation
  - natural densification at the impact location
  - better involvement of lateral material



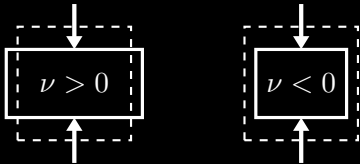
non-auxetic and auxetic materials  
(Lim 2015)



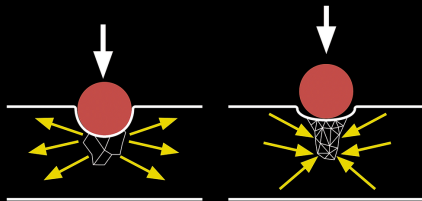
non-auxetic and auxetic material under  
impact (Kolken et al. 2017)

# Auxetic materials appear promising for impact mitigation

- auxetic materials are materials with a negative Poisson's ratio
  - materials that contract laterally when compressed
- promising capabilities for impact mitigation
  - natural densification at the impact location
  - better involvement of lateral material
- auxetic materials hardly found in nature
- assumptions don't take material architecture into account



non-auxetic and auxetic materials  
(Lim 2015)



non-auxetic and auxetic material under  
impact (Kolken et al. 2017)

# Architectures selected to ensure comparability

- Wide range of possibilities to generate auxeticity

# Architectures selected to ensure comparability



- Wide range of possibilities to generate auxeticity
- Focus on the most common for a comparison:  
Auxetic re-entrant honeycombs

# Architectures selected to ensure comparability



- Wide range of possibilities to generate auxeticity
- Focus on the most common for a comparison:  
Auxetic re-entrant honeycombs
- Stiffness and outer dimensions are kept the same:  
Conventional honeycomb in W-configuration

# Architectures selected to ensure comparability

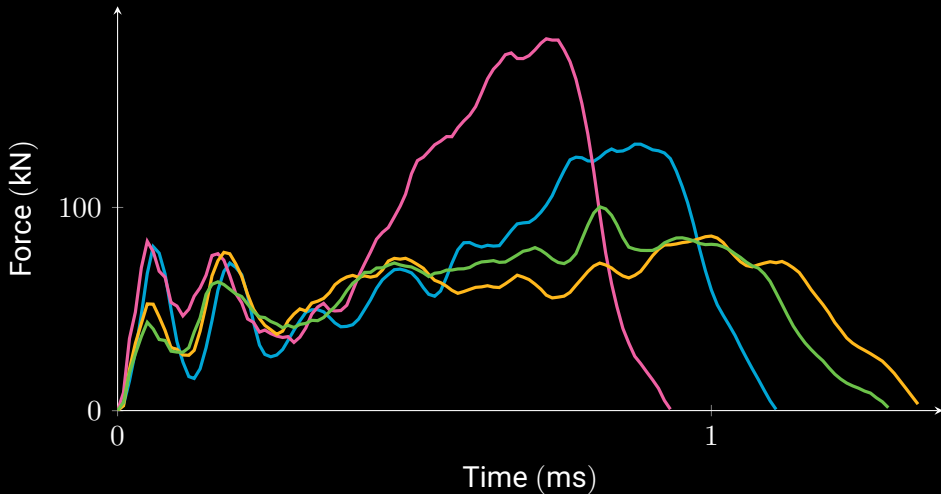


- Wide range of possibilities to generate auxeticity
- Focus on the most common for a comparison:  
Auxetic re-entrant honeycombs
- Stiffness and outer dimensions are kept the same:  
Conventional honeycomb in W-configuration  
Auxetic re-entrant honeycombs rotated by  $90^\circ$   
Conventional honeycomb in L-configuration

# Experiments show higher forces for the auxetics



# Experiments show higher forces for the auxetics



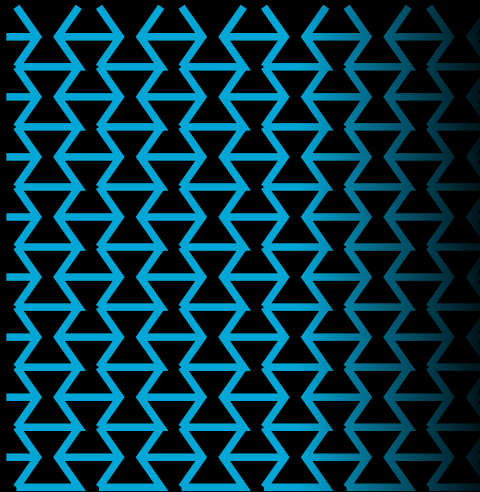


# Experiments show higher forces for the auxetics



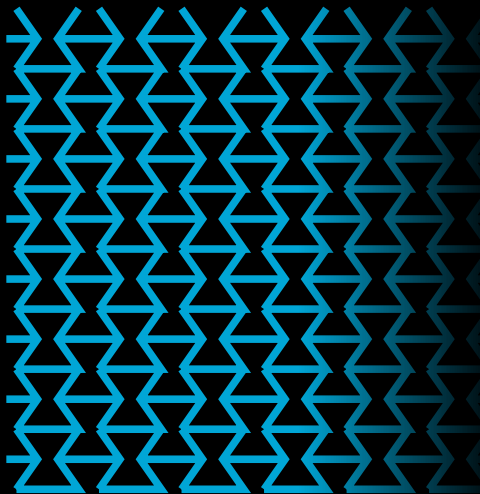
# Modelling of lattices with rods to reduce runtime

- Architectures defined as assembly of rods



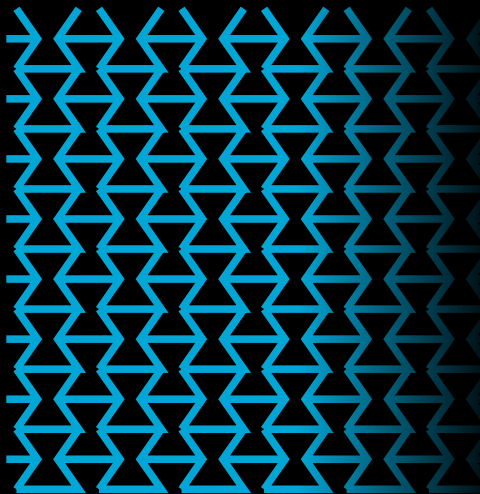
# Modelling of lattices with rods to reduce runtime

- Architectures defined as assembly of rods
- Rods represented as geometrically nonlinear Timoshenko beams
- FE-implementation of **Simo-Reissner**-elements in JEM/JIVE (C++ FE-Toolkit)



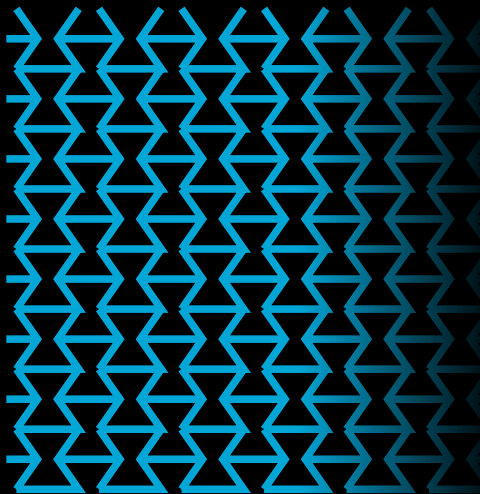
# Modelling of lattices with rods to reduce runtime

- Architectures defined as assembly of rods
- Rods represented as geometrically nonlinear Timoshenko beams
- FE-implementation of **Simo-Reissner**-elements in JEM/JIVE (C++ FE-Toolkit)
- Beam-To-Beam contact using **penalty parameters**
- Tree like contact search algorithm with exclusion of the joint elements



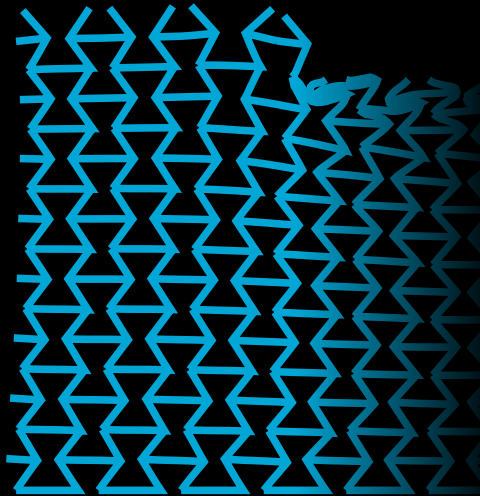
# Modelling of lattices with rods to reduce runtime

- Architectures defined as assembly of rods
- Rods represented as geometrically nonlinear Timoshenko beams
- FE-implementation of **Simo-Reissner**-elements in JEM/JIVE (C++ FE-Toolkit)
- Beam-To-Beam contact using **penalty parameters**
- Tree like contact search algorithm with exclusion of the joint elements
- Time marching with an **explicit** predictor-corrector scheme
- Time step adaptivity using a Milne-device



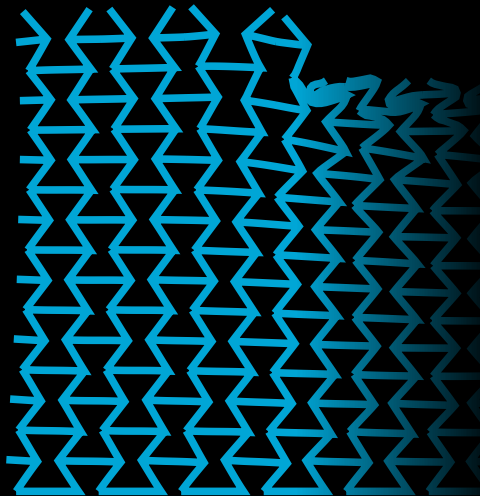
# Fast computation of geometrically nonlinear beams

- Six DOFs along the beam-axis
- Resulting in six strain prescriptors



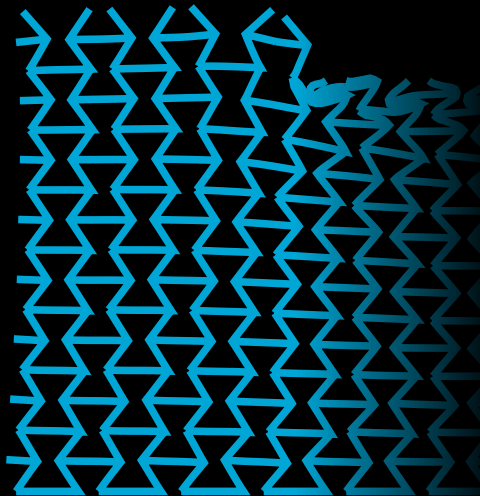
# Fast computation of geometrically nonlinear beams

- Six DOFs along the beam-axis
- Resulting in six strain prescriptors
- Linear elastic material law with six stress resultants
- Steel as material ( $E = 210 \text{ GPa}$ ,  $\nu = 0.265$ )



# Fast computation of geometrically nonlinear beams

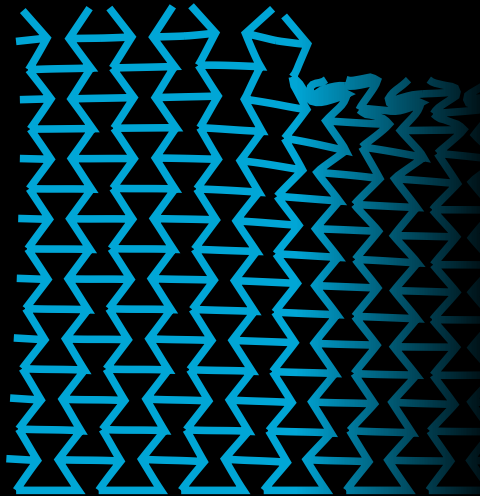
- Six DOFs along the beam-axis
- Resulting in six strain prescriptors
- Linear elastic material law with six stress resultants
- Steel as material ( $E = 210 \text{ GPa}$ ,  $\nu = 0.265$ )
- Including material nonlinearities not trivial
- Popular approach of sub-integration too slow





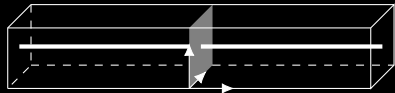
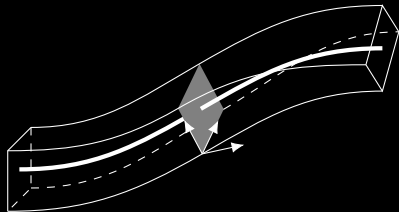
# Fast computation of geometrically nonlinear beams

- Six DOFs along the beam-axis
- Resulting in six strain prescriptors
- Linear elastic material law with six stress resultants
- Steel as material ( $E = 210 \text{ GPa}$ ,  $\nu = 0.265$ )
- Including material nonlinearities not trivial
- Popular approach of sub-integration too slow
- Possibility to model elastoplasticity on the beam-level
- Approach suggested by Smriti et al. 2018, 2020



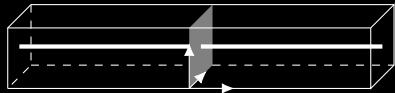
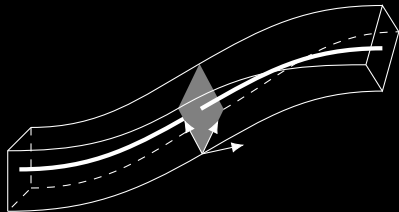
# Further speed-up with beam-type elasto-plasticity

- Yield formulated in the **stress resultant** space
- Plastic strain prescriptors fitting the beam configuration



# Further speed-up with beam-type elasto-plasticity

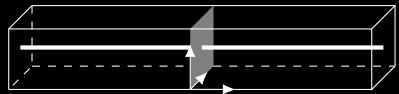
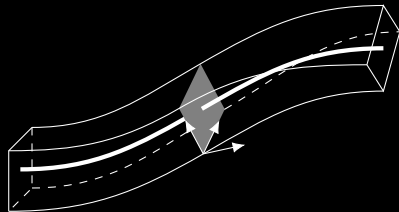
- Yield formulated in the **stress resultant** space
- Plastic strain prescriptors fitting the beam configuration
- J2-plasticity with isotropic hardening assumed on material scale
- Yield surface and hardening tensor obtained by Herrnböck et al. 2021, 2022
- Isotropic hardening on material level relates to **kinematic hardening** on beam level



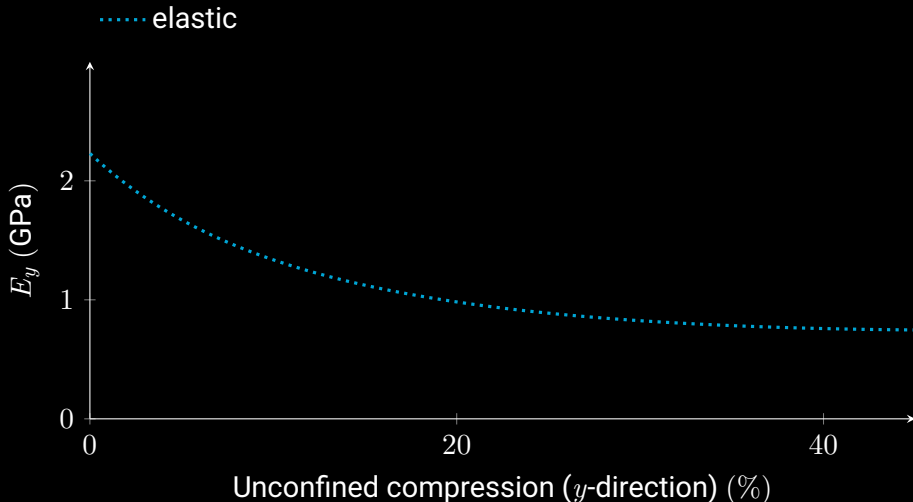
# Further speed-up with beam-type elasto-plasticity

- Yield formulated in the **stress resultant** space
- Plastic strain prescriptors fitting the beam configuration
- J2-plasticity with isotropic hardening assumed on material scale
- Yield surface and hardening tensor obtained by Herrnböck et al. 2021, 2022
- Isotropic hardening on material level relates to **kinematic hardening** on beam level
- Consistent geometric scaling of the hardening tensor introduced
- **Size-objective** formulation for the entire material model

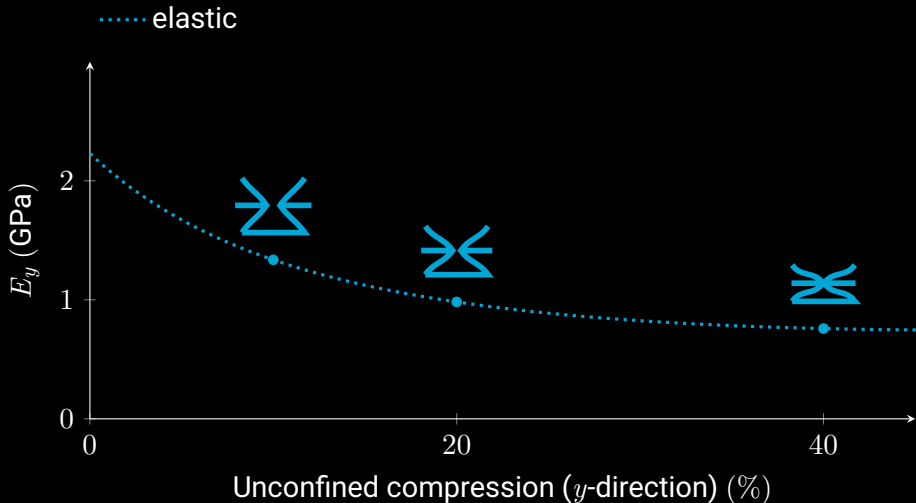
Gärtner et al. *Computational Mechanics* accepted for publication (2024)



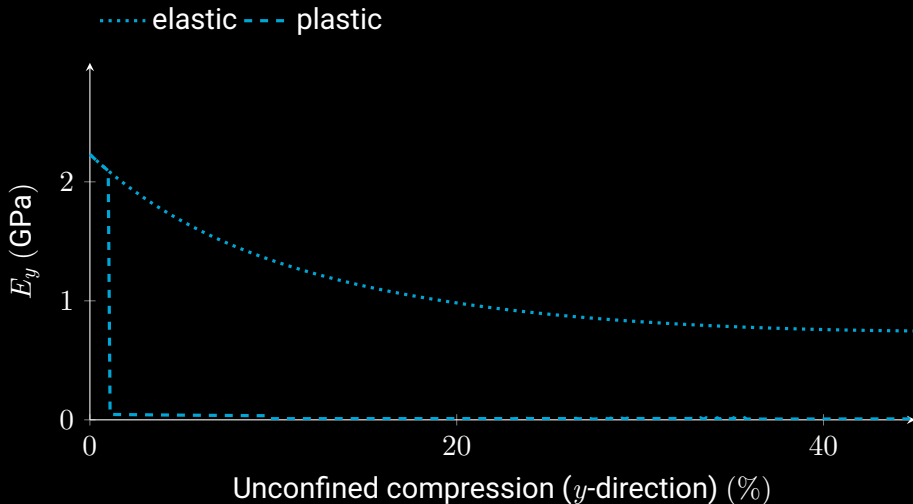
# Changes in geometry lead to changes in stiffness



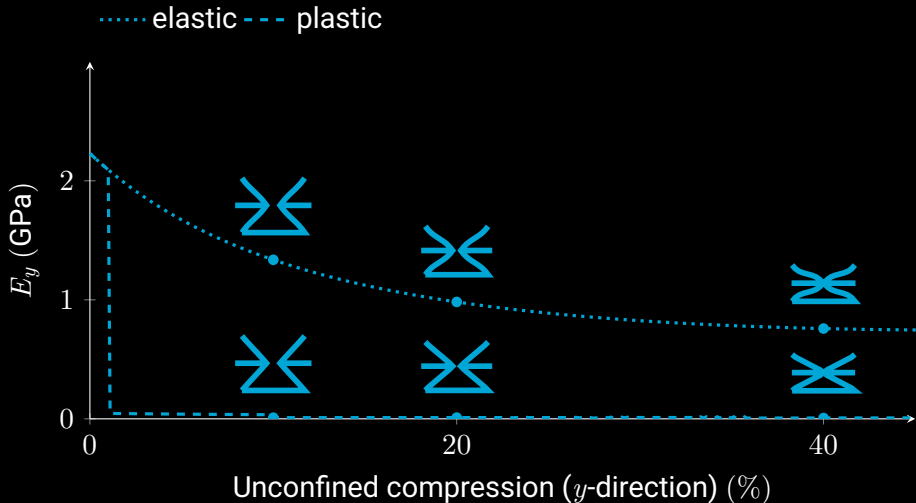
# Changes in geometry lead to changes in stiffness



# Plasticity leads to free hinging of the joints

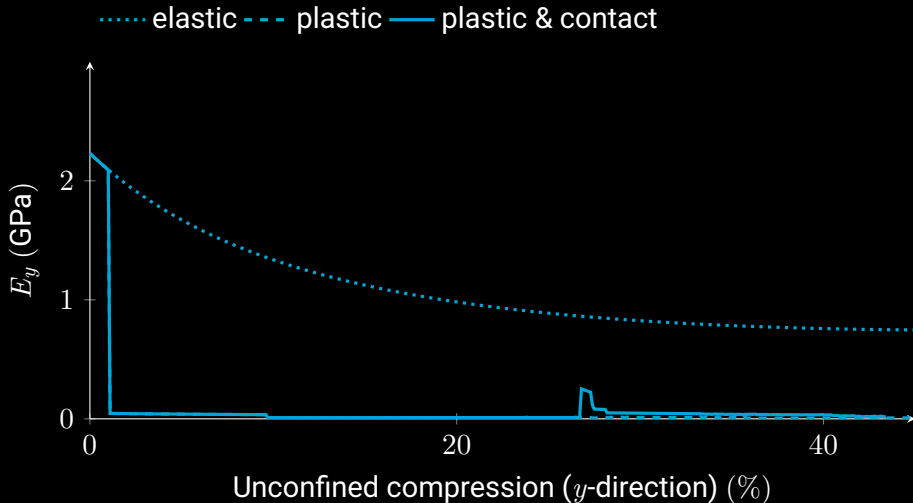


# Plasticity leads to free hinging of the joints

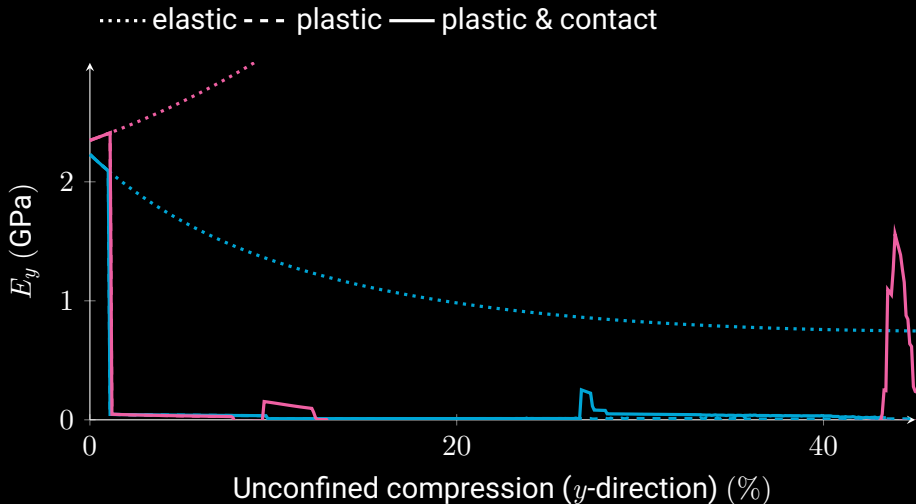




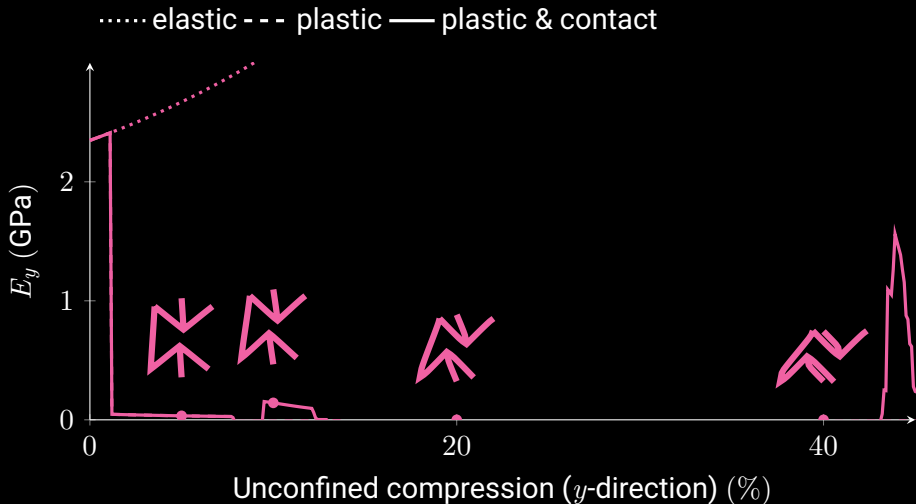
# Contact has little influence on the further behavior



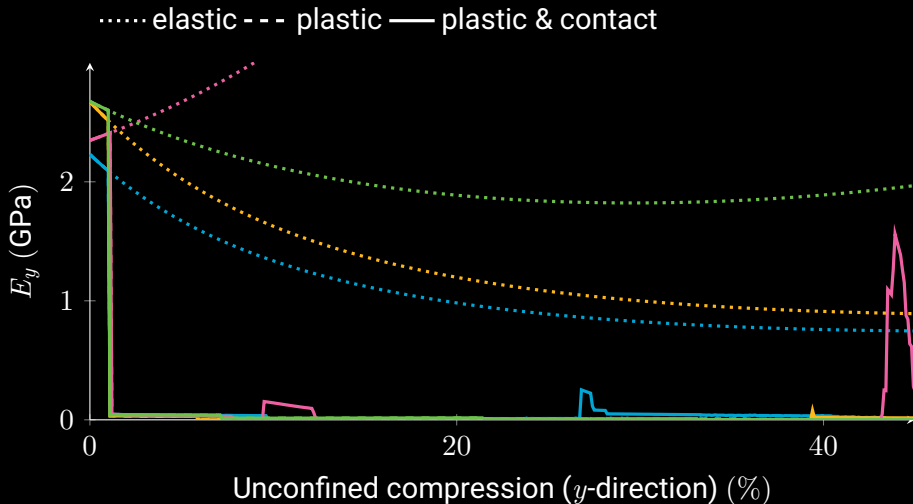
# Plasticity can induce buckling



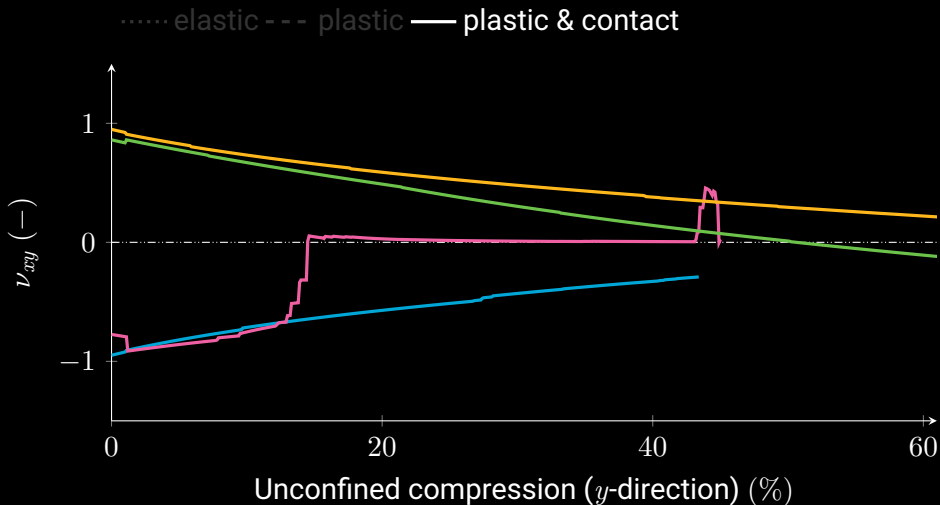
# Plasticity can induce buckling



# Development of stiffness differs for architectures

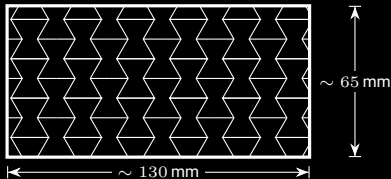


# Poisson's ratio tends to 0 with compression



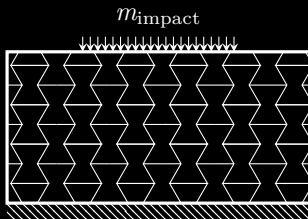
# Impact compression tests

- Impact simulation conducted with patches of  $\sim 130 \text{ mm} \times 65 \text{ mm}$



## Impact compression tests

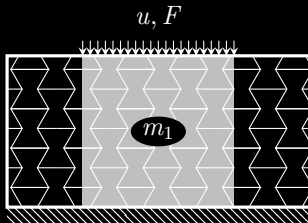
- Impact simulation conducted with patches of  $\sim 130 \text{ mm} \times 65 \text{ mm}$
- An impactor of 1.2 kg is emulated at the top with an initial speed of  $70 \text{ m s}^{-1}$
- Apply the impact at the middle patch 65 mm wide



# Impact compression tests

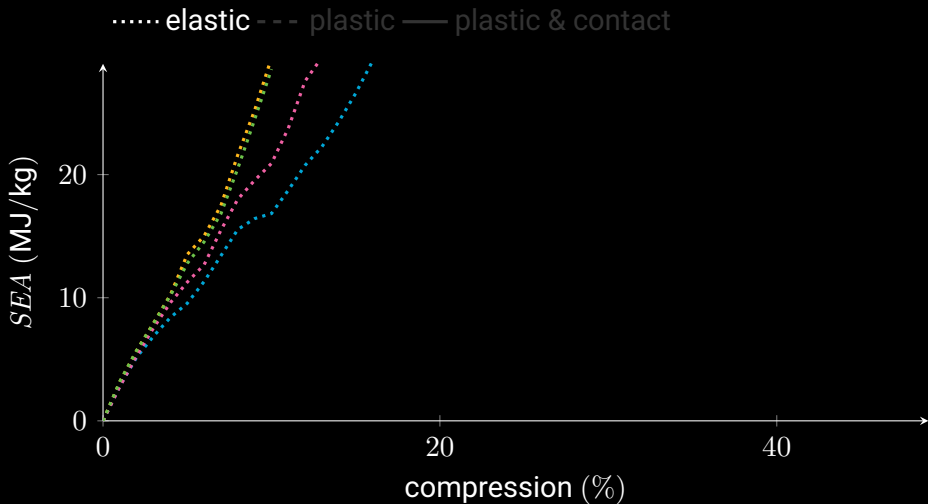
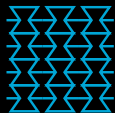
- Impact simulation conducted with patches of  $\sim 130 \text{ mm} \times 65 \text{ mm}$
- An impactor of 1.2 kg is emulated at the top with an initial speed of  $70 \text{ m s}^{-1}$
- Apply the impact at the middle patch 65 mm wide
- Evaluating force over the middle patch
- Evaluating the specific energy absorption (SEA)

$$\text{SEA} = \frac{1}{m_1} \int F \, du$$

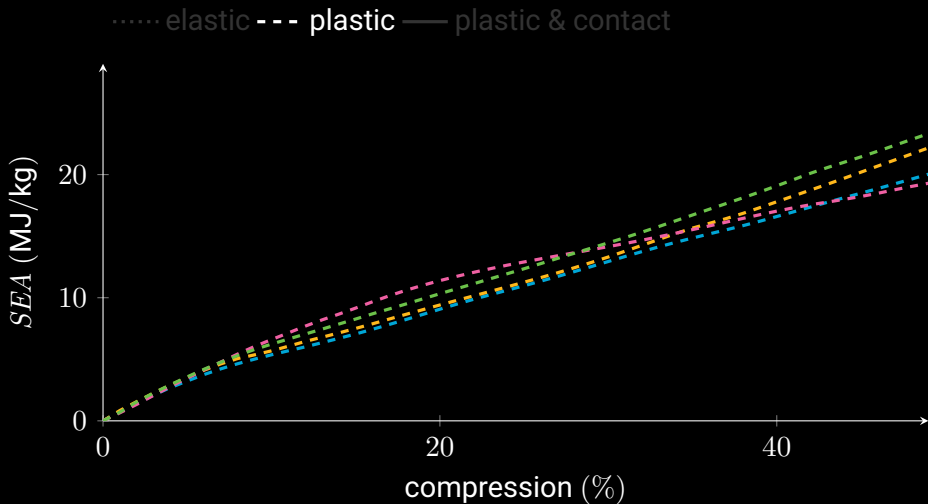
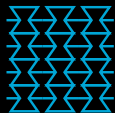




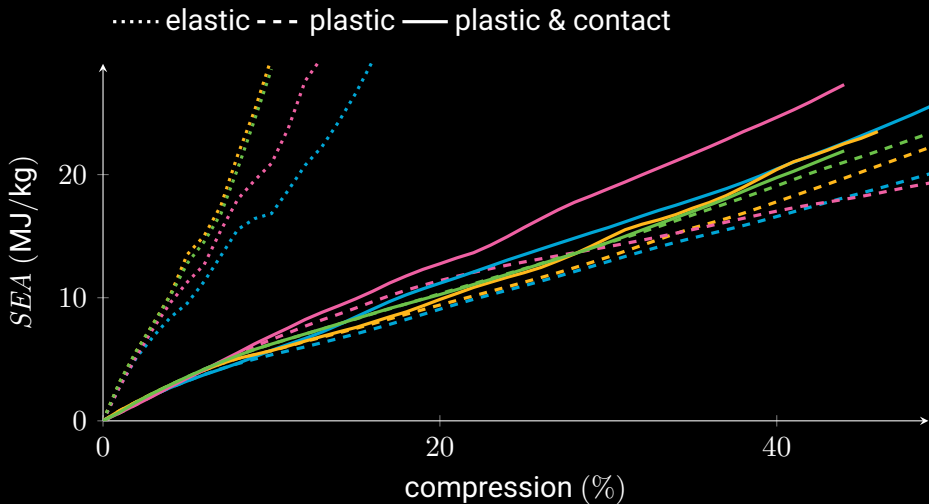
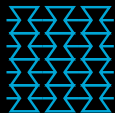
# Impact Tests – Influence of material nonlinearities



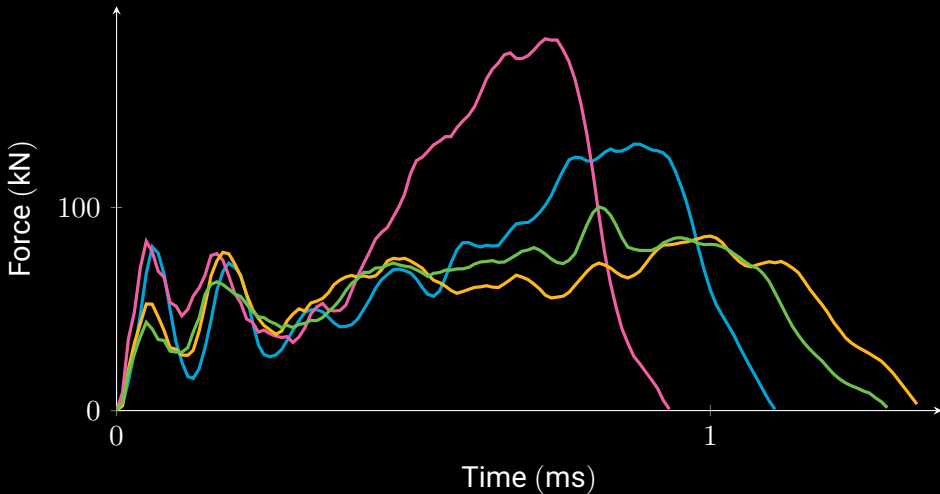
# Impact Tests – Influence of material nonlinearities



# Impact Tests – Influence of material nonlinearities

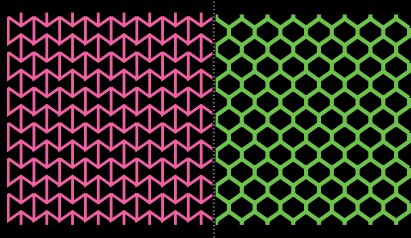
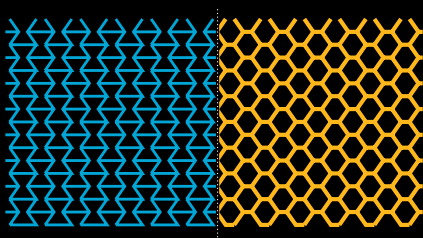


# Impact Tests – Influence of material nonlinearities



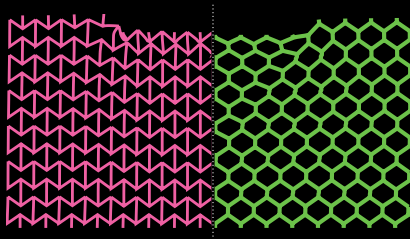
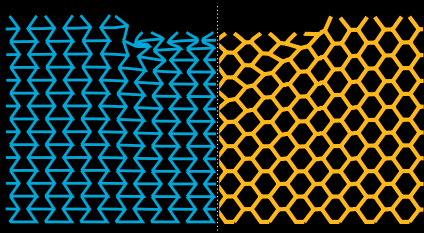
# Conclusions

- Lattice materials as such do not follow linear continuum assumptions



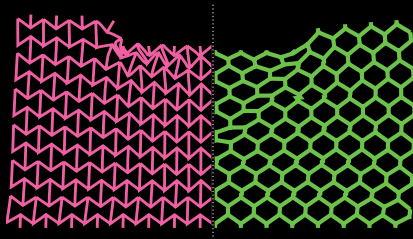
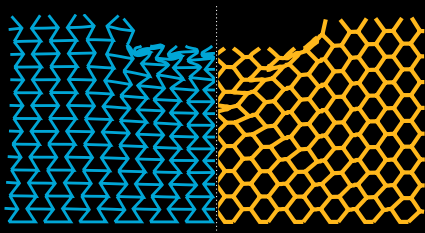
# Conclusions

- Lattice materials as such do not follow linear continuum assumptions
- Interaction between material and geometric nonlinearities crucial



# Conclusions

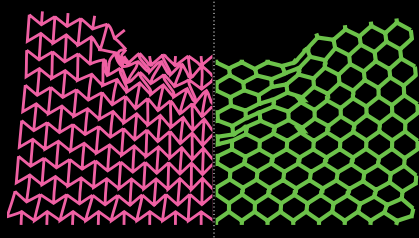
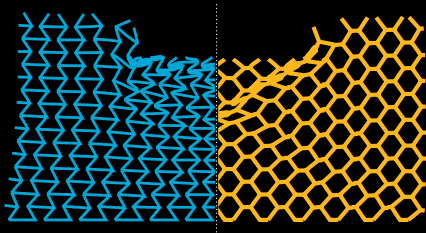
- Lattice materials as such do not follow linear continuum assumptions
- Interaction between material and geometric nonlinearities crucial
- Plasticity leads to stronger localization of the deformation
  - ⇒ Dependency on architecture under investigation



# Conclusions

- Lattice materials as such do not follow linear continuum assumptions
- Interaction between material and geometric nonlinearities crucial
- Plasticity leads to stronger localization of the deformation
  - ⇒ Dependency on architecture under investigation
- Auxetic structures lead to temporal and spatial concentration of forces
  - ⇒ Have a look at the poster as well!

Gärtner, Dekker, van Veen, van den Boom, and Amaral *publication in preparation*







**Thank you!**  
**Comments?**

# References I

- [1] Teik-Cheng Lim. *Auxetic Materials and Structures*. Engineering Materials. Singapore: Springer Singapore, 2015.
- [2] H. M. A. Kolken and A. A. Zadpoor. "Auxetic mechanical metamaterials". In: *RSC Adv.* 7 (9 2017), pp. 5111–5129.
- [3] Smriti, Ajeet Kumar, Alexander Großmann, and Paul Steinmann. "A thermoelastoplastic theory for special Cosserat rods". In: *Mathematics and Mechanics of Solids* 24.3 (2018).
- [4] Smriti, Ajeet Kumar, and Paul Steinmann. "A finite element formulation for a direct approach to elastoplasticity in special Cosserat rods". In: *International Journal for Numerical Methods in Engineering* 122.5 (2020).
- [5] Ludwig Herrnböck, Ajeet Kumar, and Paul Steinmann. "Geometrically exact elastoplastic rods: determination of yield surface in terms of stress resultants". In: *Computational Mechanics* 67.3 (2021).

## References II

- [6] Ludwig Herrnböck, Ajeet Kumar, and Paul Steinmann. “Two-scale off-and online approaches to geometrically exact elastoplastic rods”. In: *Computational Mechanics* 71.1 (2022).
- [7] Til Gärtner, Sanne J. van den Boom, J. Weerheijm, and L. J. Sluys. “A Strategy for Scaling the Hardening Behavior in Finite Element Modelling of Geometrically Exact Beams”. In: *Computational Mechanics* (2024). accepted for publication.
- [8] Til Gärtner, S. J. van den Boom, J. Weerheijm, and L. J. Sluys. “Geometric effects on impact mitigation in architected auxetic metamaterials”. In: *Mechanics of Materials* 191 (2024), p. 104952.
- [9] Til Gärtner, Richard Dekker, Dennis van Veen, Sanne J. van den Boom, and Lucas Amaral. “(In)Efficacy of Auxetic Metamaterials for Impact Mitigation: Investigations of Energy Absorption and Force Distribution”. publication in preparation. 2024.